

Bending-active structures: a review of design principles

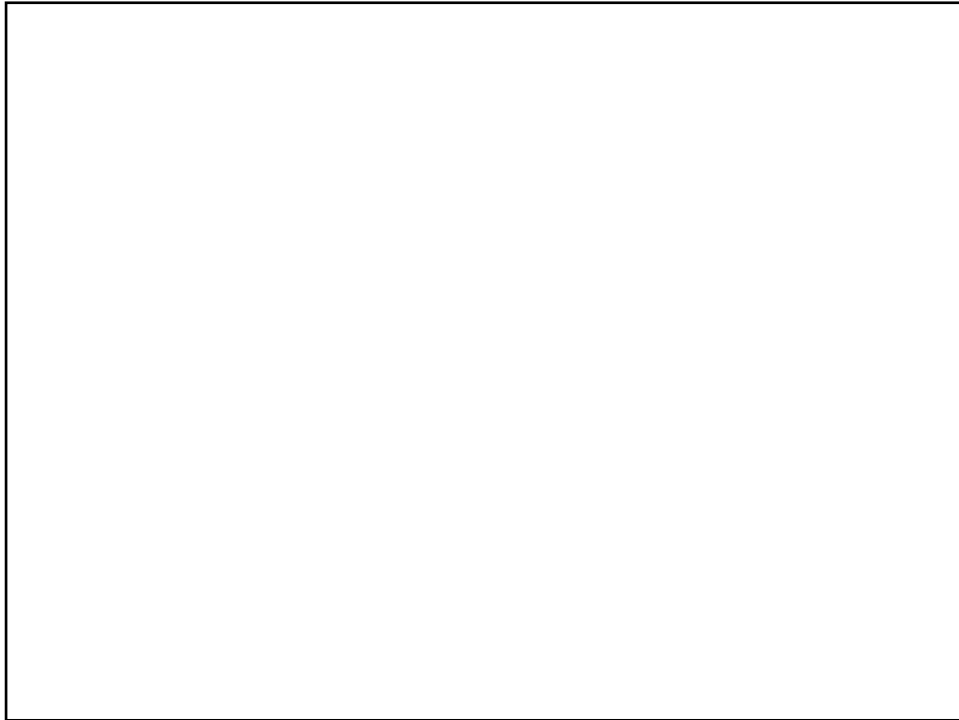
Stijn Brancart
Tuesday 17 Oct 2017



Active bending is the systemic use of elastic deformation

"Bending-active structures are *structural systems* that include curved beam or shell elements that base their geometry on the *elastic deformation* from an initially straight or planar configuration."

Knippers et al. (2011) - Construction manual for polymers + membranes
Lienhard et al. (2013) - Active Bending, a review on structures where bending is used as a self-formation process



Existing structures are very varied but do touch some common design principles



Existing structures are very varied but do touch some common design principles

Restraint techniques

define how bending is induced and maintained in the system

Stiffening techniques

define how stiffness is developed withing the system

1. Introduction

2. Elastic formation in design and construction

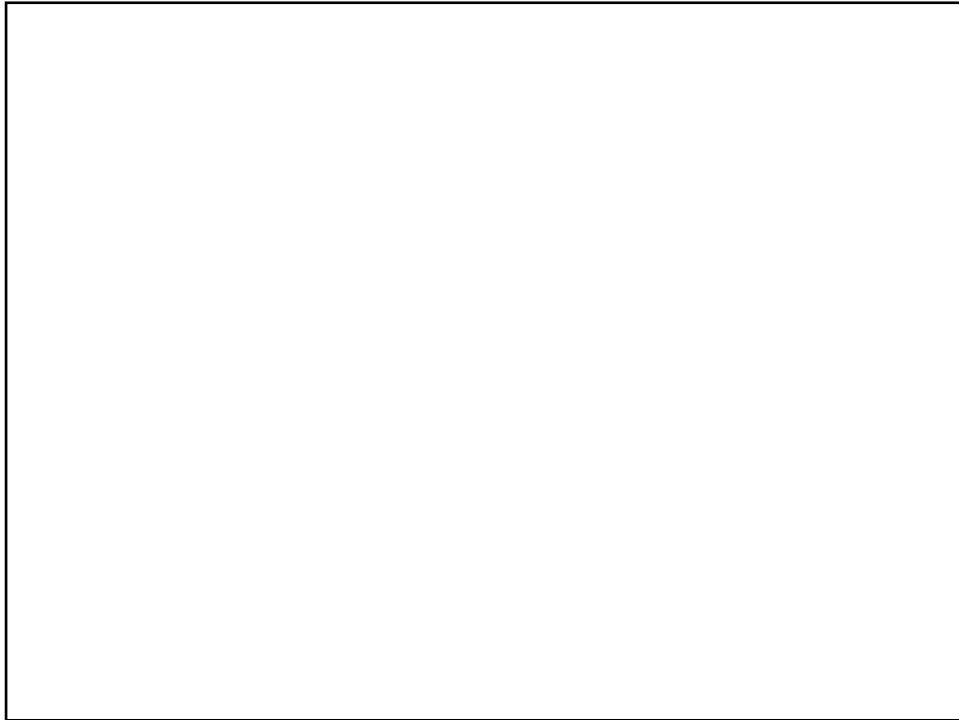
3. Form through force: restraining bending-active systems

Pre-bent members
Self-restraining system
Post-restrained structure

4. Stiffness through flexibility: manipulating elastic behaviour

Elastic stiffness
Initial displacement stiffness
Geometric stiffness

5. Conclusions



Existing structures differ in the way bending is induced and maintained in the system

Pre-bent components
can be pre-assembled in the workshop

Self-restraining systems
maintain bending through the component interaction

Post-restrained structures
can be assembled on the ground

Pre-bent components can be pre-assembled in the workshop



a. ReciPlyDome - KADK + Vrije Universiteit Brussel



b. Dermoid - CITA + SIAL



c. ICD/ITKE pavilion 2015-2016
University of Stuttgart

Self-restraining systems maintain bending through the component interaction



d. Panikkar - CODA

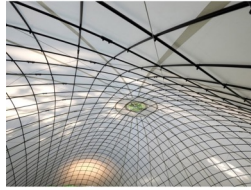


e. ICD/ITKE pavilion 2010 -
University of Stuttgart



f. Undulatus -
Vrije Universiteit Brussel

Post-restrained structures can be assembled on the ground



g. SheltAir - UdK Berlin

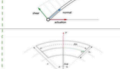
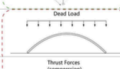
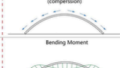
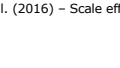


h. TorUs - CODA



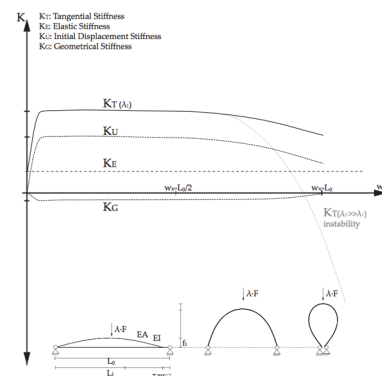
i. Pavilion - EmTech (AA) + ETH

The stiffness is defined by three components:
elastic, initial displacement and geometric stiffness

	Bending	Thickness h	Variable: span s	Thickness	Scale
Moment required for bending		$M_B = \frac{EI}{r^3} = \frac{E \cdot b \cdot h^3}{12 \cdot r^3}$	$M_B = \frac{EI}{12 \cdot r^3} = \frac{E \cdot s \cdot b \cdot (h/2)^3}{12 \cdot r^3}$	$M_B \propto h^3$	s^3
Normal stress due to bending		$\sigma_{NB} = \frac{M_B}{I} = \frac{M_B}{b \cdot h^3/12}$, $N_B \propto h^3$	$\sigma_{NB} = \frac{M_B}{I} = \frac{M_B}{b \cdot h^3/12}$, $N_B \propto s^3$	$\sigma_{NB} \propto h^2$	s
Flexural stress due to bending		$\sigma_{NB} = \frac{E \cdot h}{2 \cdot r}$	$\sigma_{NB} = \frac{E \cdot s \cdot b}{2 \cdot r^3}$	$\sigma_{NB} \propto h$	1
Axial force from dead load				$N_D \propto h$	s^3
Axial stress from dead load		$\sigma_{ND} = \frac{N_D}{A} = \frac{N_D}{b \cdot h}$, $N_D \propto h$	$\sigma_{ND} = \frac{N_D}{A} = \frac{N_D}{b \cdot h}$, $N_D \propto s^3$	$\sigma_{ND} \propto 1$	s
Deflection from dead load		$w_{relative} = \frac{M_B}{EI} = \frac{12M_B}{E \cdot b \cdot h^3}$, $M_B \propto h$	$w_{relative} = \frac{1}{12} \frac{12M_B}{E \cdot b \cdot h^3} = \frac{12M_B}{E \cdot b \cdot h^3}$, $M_B \propto s^3$	$w_{relative} \propto h^{-2}$	s

Takahashi et al. (2016) – Scale effect in bending-active plates and a novel concept for elastic kinetic roof systems

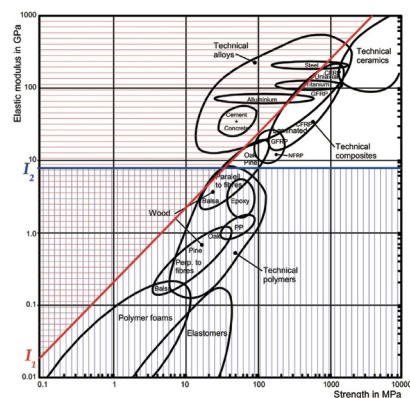
The stiffness is defined by three components:
elastic, initial displacement and geometric stiffness



Lienhard (2014) – Bending-active structures, form-finding strategies using elastic deformation in static and kinematic systems and the structural potential therein

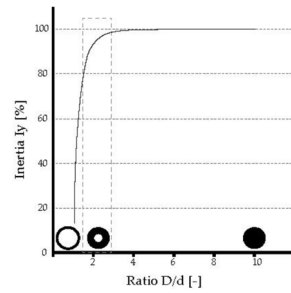
The elastic stiffness is constant throughout the deformation

Materials for active bending should have high elasticity to strength ratios



Kotelnikova-Weiler et al. (2013) - Materials for actively-bent structures

Cross-sections and component geometry define stiffness and residual stress



$$\frac{1}{r} = \frac{M}{E \cdot I} \quad (1)$$

$$\sigma = \frac{E \cdot I}{r \cdot w} = \frac{E \cdot t}{2 \cdot r} \quad (2)$$

Ahlquist & Lienhard (2016) - Extending Geometric and Structural Capacities for Textile Hybrid Structures with Laminated GFRP Beams and CNC Knitting

Lienhard, Schleicher & Knippers (2011) - Bending-active structures - Research Pavilion ICD/ITKE

Manipulating the components allows customising for a certain geometry or behaviour



EmTech (AA) - ETH pavilion

Kerf-based complex wood systems - Achim Menges

Anisotropic properties can be interesting when separating direction of bending from loading



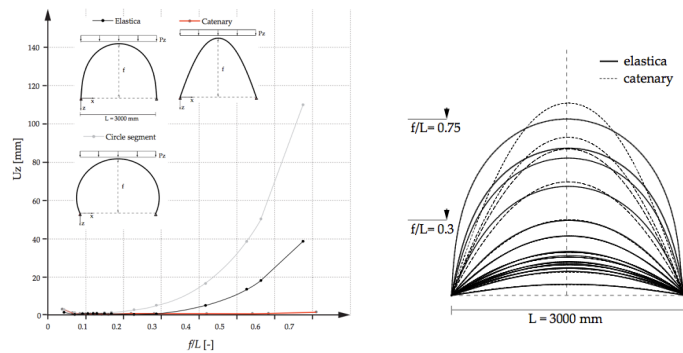
Neula - CODA



TorUs - CODA

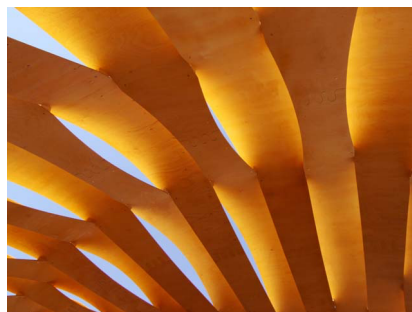
The initial displacement stiffness is defined by the deformed geometry

Different curved geometries lead to varying load-bearing behaviour

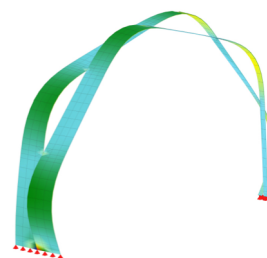


Lienhard (2014) - Bending-active structures, form-finding strategies using elastic deformation in static and kinematic systems and the structural potential therein

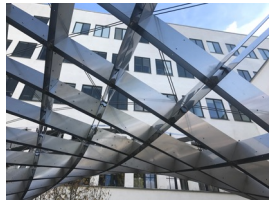
Coupling can improve the behaviour by increasing the structural height



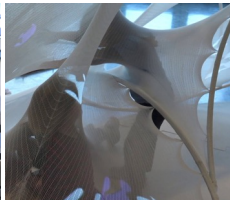
ICD/ITKE research pavilion 2010



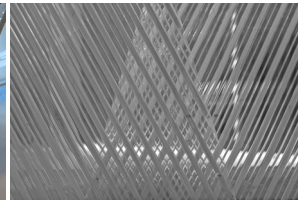
Coupling can increase the moment of inertia while maintaining the residual stress



Layering
Asymptotic pavilion – Eike Schling



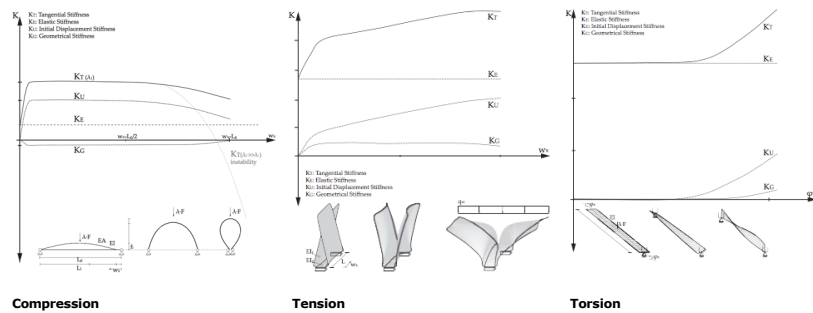
Bundling
Sensory Playscape – Sean Ahlquist



Insertion
TwoDtoThreeD – KOGE (Günther Filz)

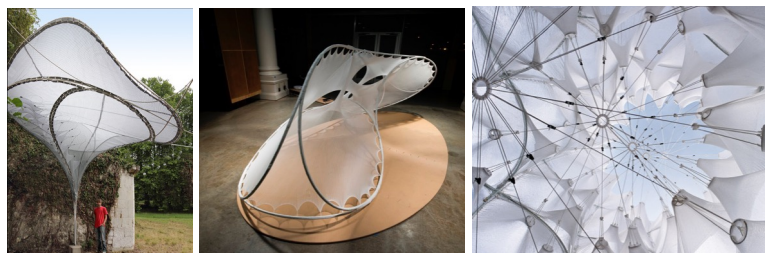
The geometric stiffness is the result of the stress-stiffening effect

The stress-stiffening is defined by the flow of forces



Lienhard (2014) - Bending-active structures, form-finding strategies using elastic deformation in static and kinematic systems and the structural potential therein

Tension can increase the stiffness of bending-active (hybrid) structures considerably



M1 Tour de l'architecte – Lienhard & Ahlquist

Sensory Playscape – Sean Ahlquist

Hybrid Tower – Udk (Berlin) + CITA (Copenhagen)

